

Numerical Methods for Geosciences: Building an Earthquake Cycle Model

Fridays 10:30–12:30, Sept 2026–Jan 2027 (Salle E509)

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This course aims at training students in numerical methods in geosciences. While the topic is very vast, in the interest of making it useful and goal-oriented, we have decided to build an earthquake-cycle model by the end of the course. The course is about learning aspects of numerical methods based on the tools needed to build this model — root-finding and time integration schemes to handle the governing nonlinear equations; finite differences and finite volumes to solve the thermal pressurization diffusion problem on the fault; and boundary element methods to compute the elastic interaction between fault patches. These pieces are then coupled together, with dilatancy and adaptive time-stepping added, to assemble a working quasidynamic earthquake-cycle simulator on a 1D fault. Each theoretical lecture is paired with a hands-on coding session in Python, so that by the end of the semester students will have built, from scratch, every component of a functioning numerical model of the earthquake cycle.

Each topic gets a full 2h theory Friday and, the following Friday, a full 2h coding Friday — a week apart. Every coding session opens with a short recap of the prior week’s theory before students start writing code.

Session calendar

#	Date	Type	Topic
1	Fri 11 Sep 2026	Theory	Foundations — root-finding & time integration
2	Fri 18 Sep 2026	Coding	Foundations
3	Fri 09 Oct 2026	Theory	FD — thermal pressurization I
4	Fri 16 Oct 2026	Coding	FD
5*	Fri 23 Oct 2026	Theory	FV — thermal pressurization II
6*	Fri 30 Oct 2026	Coding	FV
7	Fri 06 Nov 2026	Theory	BEM — elastic interaction matrix
8	Fri 13 Nov 2026	Coding	BEM
9	Fri 20 Nov 2026	Theory	Coupling — mechanics + TP + dilatancy + adaptive integration
10	Fri 04 Dec 2026	Coding	Coupling
11	Fri 11 Dec 2026	Theory	Synthesis — multi-patch assembly & benchmarking
12	Fri 18 Dec 2026	Coding	Synthesis

- Vacances de la Toussaint

Sessions 1–2 — Foundations: root-finding & time integration

Session 1 (Theory, 2h)

- Rate-and-state friction law inversion via Newton–Raphson: derivation, convergence, why a log- V initial guess behaves better than a raw- V one.
- A proper numpy/vectorization review — array ops, functions, plotting — this pays off directly in Sessions 7–8 (assembling and multiplying the stiffness matrix) and Sessions 9–10 (coupling), where shaky fundamentals would otherwise slow things down.
- Explicit ODE integration: Euler from a Taylor expansion, then RK4.
- The single-DOF spring-slider system: $dt/dt = k(V_{load} - V)$, V solved via Newton each step.

Session 2 (Coding, 2h)

- Recap (10–15 min): Newton’s method and RK4, core ideas only.
- Newton solver + friction-law wrapper.
- RK4 integrator; run the baseline spring-slider, plot $V(t)$.

Sessions 3–4 — FD: thermal pressurization I

Session 3 (Theory, 2h)

- Mechanism: frictional heating $q = \tau V$ at the fault plane drives 1D diffusion of temperature and pore pressure perpendicular to the fault; pore-pressure rise reduces effective normal stress, weakening the fault (Rice, 2006).
- Full derivation of the FD scheme: discretize the perpendicular (y) direction, central-difference the second derivative, explicit (FTCS) vs. implicit (backward Euler, tridiagonal solve) time-stepping.
- Stability, derived properly: von Neumann analysis, the diffusion number, and why implicit will matter once this couples to a fast-accelerating slip velocity.
- Boundary conditions: source at $y = 0$, effectively-infinite far-field condition.

Session 4 (Coding, 2h)

- Recap: the diffusion equation and the FD scheme.
 - Build a 1D FD diffusion solver for $T(y,t)$ given a prescribed heating history $q(t)$ at $y=0$.
 - Validate against the analytic Green's-function solution for a delta-function heat pulse.
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Sessions 5–6 — FV: thermal pressurization II

Session 5 (Theory, 2h)

- Full control-volume / flux-balance derivation of the same diffusion equation — same result as Session 3, different route.
- Why FV handles a spatially varying diffusivity properly (a diffusivity contrast between fault-core and damage-zone material) where naive FD needs care.
- Work through the uniform-diffusivity case (should agree with FD) and a diffusivity-jump case.

Session 6 (Coding, 2h)

- Recap: control-volume derivation, where FD and FV should and shouldn't agree.
 - Rewrite the diffusion solver in flux-conservative FV form.
 - Run both on a spatially varying diffusivity profile and compare.
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Sessions 7–8 — BEM: the elastic interaction matrix

Session 7 (Theory, 2h)

- Discretizing the 1D fault into N patches of slip.
- Full derivation of the elastic dislocation kernel for a 1D fault — From first principles rather than handing it over as a formula, especially if students haven't taken the earthquake source mechanics course.
- Assemble into a stiffness matrix K ($N \times N$): symmetry, the self-stiffness diagonal term, why nearby patches dominate the interaction.

Session 8 (Coding, 2h)

- Recap: the kernel derivation and matrix structure.
 - Validate on a simple two-patch symmetric case.
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Sessions 9–10 — Coupling: mechanics, thermal pressurization, dilatancy & adaptive integration

Session 9 (Theory, 2h) — the pinch-point lecture; it now gets the room it deserves.

- Full per-patch picture: elastic stress from K (BEM) -> root-find V from the friction law using an *effective* normal stress $\sigma_{\text{eff}} = \sigma_n - p$ (not the constant σ_n from Session 1) -> frictional heat $q = \tau V$ feeds the diffusion solver -> updated p feeds back into σ_{eff} next step.
- Why this feedback loop (heat -> pressure -> weakening -> faster slip -> more heat) is stiffer than the Session 1.
- Dilatancy as a second, competing feedback: gouge porosity ϕ relaxes toward a velocity-dependent steady state over the same critical slip distance D_c already used in the friction law — structurally the same relaxation-ODE pattern as the state variable θ from Session 1, just applied to porosity instead of friction state. Point this out explicitly; it's new physics.
- Operator splitting, worked by hand on the board with a small 2-coupled-ODE example before touching the real system: advance the mechanical ODE one step with the current p , then advance the diffusion solve (now with both the heating source and the dilatant sink) one step, alternate.

Session 10 (Coding, 2h)

- Recap: the feedback loop, the splitting scheme, and the two competing pressure terms — referring back to the board example.
 - Wire in a diffusion module FD or FV, student's choice, same interface — behind the friction/root-finding step.
 - Add the porosity state variable and its relaxation ODE; feed the dilation rate into the diffusion sink term.
 - Re-run the Session 1–2 spring-slider three ways: dry baseline, TP only, TP + dilatancy — compare all three directly.
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Sessions 11–12 — Synthesis: full multi-patch assembly and benchmarking

Session 11 (Theory, 2h)

- Extending the Session 9–10 feedback loop to N patches: each patch carries its own independent local diffusion state and its own porosity state (a small perpendicular grid per patch), coupled to the others only through the elastic stress-transfer matrix — not directly coupled in the perpendicular direction. Diffusion solves stay embarrassingly parallel: one independent tridiagonal system per patch, per step.
- Diagnostics: moment-rate function, recurrence interval, and a meaningful dry / TP-only / TP+dilatancy comparison across the whole fault — this is where dilatancy's stabilizing role against thermal weakening actually becomes visible at the cycle scale, not just the single-patch scale from Session 10.
- Benchmarking: the single-patch limit should recover the Session 9–10 result; check simulated nucleation length against the analytic h^* estimate.

Session 12 (Coding, 2h) — This is where all six prior pieces complexify, and bugs are hardest to isolate without dedicated time.

- Recap: multi-patch extension and the diagnostics to compute.
 - Assemble: N patches, each with its own diffusion and porosity state, coupled via elasticity, driven by the Session 9 RHS.
 - Run at moderate N (~ 50), produce moment-rate/recurrence plots for the dry, TP-only, and TP+dilatancy cases side by side.
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